



(19) Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) EP 1 004 684 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
31.05.2000 Bulletin 2000/22

(51) Int. Cl.⁷: C22C 19/05, B23K 35/00 RECEIVED

JUN 22 2005

IPO
GENERAL ELECTRIC CO.

(21) Application number: 99308723.8

(22) Date of filing: 03.11.1999

(84) Designated Contracting States:
AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU
MC NL PT SE
Designated Extension States:
AL LT LV MK RO SI

• Mukira, Charles Gitahi
Watervliet, New York 12189 (US)
• Ritter, Ann Melinda
Niskayuna, New York 12309 (US)
• Crimi, Paul Vincent
Oldsmar, Florida 34677 (US)
• White, Raymond Alan
Schenectady, New York 12306 (US)

(30) Priority: 24.11.1998 US 198633

(71) Applicant:
GENERAL ELECTRIC COMPANY
Schenectady, NY 12345 (US)

(74) Representative:
Szary, Anne Catherine, Dr. et al
GE London Patent Operation,
Essex House,
12-13 Essex Street
London WC2R 3AA (GB)

(72) Inventors:

• Jackson, Melvin Robert
Niskayuna, New York 12309 (US)
• Frost, Aaron Todd
Ballston Spa, New York 12020 (US)

(54) Alloy for repairing turbine blades and their components, process thereof and the repaired article

(57) A composition comprises cobalt; chromium; carbon; boron; zirconium; aluminum; at least one refractory material; and nickel. The composition is used as a

repair material for repairing superalloy articles in a repair process.

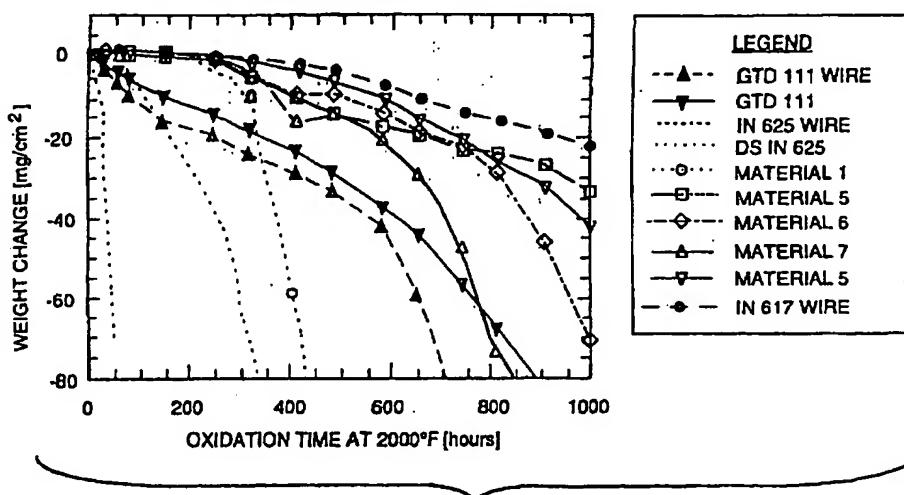


FIG. 1

Description

[0001] The invention relates to compositions of matter. In particular, the invention relates to compositions of matter that are usable for the repair of turbines and their components.

5 [0002] Turbines, airfoils, vanes, buckets, blades, nozzles, and like elements and their components (hereinafter "turbine components"), are used in high pressure applications.

[0003] Turbine components are often formed from superalloy materials. Superalloy materials possess desirable oxidation and corrosion resistance, resistance to thermal fatigue cracking, and high strength. One known superalloy material is GTD111 (a nickel-based superalloy having a composition in approximate weight percent comprising 14% 10 chromium (Cr), 9.5% cobalt (Co), 3.8% tungsten (W), 1.5% molybdenum (Mo), 4.9% titanium (Ti), 3.0% aluminum (Al), 0.1% carbon (C), 0.01 % boron (B), 2.8% tantalum (Ta), and a balance (BAL) of nickel (Ni)). The GTD111 material, when used in turbine components, is provided with one of an equiaxed (EA), single crystal, and directionally solidified (DS) microstructure.

[0004] Turbine components suffer damage and degradation during service such as often occurs at a turbine 15 bucket's tip. This degradation includes serious material loss at a trailing edge of the tip. The material loss is due, at least in part, to oxidation and hot corrosion damage, as well as thermal fatigue cracking of the material.

[0005] A damaged turbine component must be repaired if it is to return to service. In the past, a damaged turbine 20 component, for example a turbine bucket with a damaged tip, has had the tip ground away to a depth approximately equal to a turbine bucket tip cover plane. A new turbine bucket tip is built up on the cover plane by a multiple weld-pass repair process, in which the repair material is fed into the weld pool as the pool is moved around the perimeter of a cover tip on the turbine component and melted thereon to form a new tip.

[0006] One such turbine component weld repair process comprises repairing by welding without both pre-heating 25 of the turbine component and continued heating of the turbine component during the repair process. The repair material for such a turbine component weld repair process often uses a nickel-based superalloy repair material, especially if the turbine component is formed from a nickel-based superalloy material. For example, one nickel-based superalloy repair material comprises IN625 (a nickel-based superalloy having a composition in approximate atomic percent comprising 24.64% chromium (Cr), 5.6% molybdenum (Mo), 0.25% titanium (Ti), 0.44% aluminum (Al), 0.25% carbon (C), 2.1% iron (Fe), 2.3% niobium (Nb) and a balance (BAL) of nickel (Ni)). IN625 nickel-based superalloy possesses acceptable weld adherence and mechanical compatibility with a superalloy turbine material, such as a GTD111 nickel-based 30 superalloy. Welds comprising IN625 repair material on a turbine component, such as a GTD111 turbine component, exhibit a low cracking frequency following a weld repair process. Further, a repaired turbine component comprising IN625 repair material exhibits low cracking frequency after subsequent heat treatments, which is a desirable turbine component characteristic.

[0007] An IN625 repair material, while exhibiting low crack frequency, possesses undesirable strengths and oxidation 35 resistance in a repaired turbine component and so can only be used to repair turbine components subjected to moderated temperatures and times encountered in high pressure and temperature turbine component usage. Therefore, a GTD111 repair material was investigated as a weld repair material for repairing a GTD111 turbine component. A repair process using GTD111 repair material heats the turbine component prior to, and during, the weld repair process. The turbine component temperature reaches temperatures greater than about 950°C during heating to avoid forming cracks in the turbine component and repair material. The cracking would require undesirable re-work of a once-repaired turbine component, and may not correct or eliminate cracking problems in the repaired turbine components, which, of course, is undesirable.

[0008] A turbine component repaired with a GTD111 produces an enhanced strength weld repair when compared 45 to a turbine component repaired with IN625. A repaired turbine component comprising a GTD111 is more oxidation resistant than IN625, but is prone to oxidation since its oxidation resistance is only as much as the original turbine component material's oxidation resistance. While a repaired turbine component with GTD111 exhibits enhanced oxidation resistance compared to that of a repaired turbine component with IN625, the oxidation resistance is not as high as desirable.

[0009] Accordingly, a crack and oxidation resistant repair material for repairing turbine components is needed. The 50 repair material should not require additional heating of the turbine component for repair, because of the undesirable cracking effects associated with heating. Further, the repair material should be more oxidation resistant than known repair materials, such as, but not limited to, IN625 and GTD111, and be as strong as or stronger than IN625.

SUMMARY OF THE INVENTION

55

[0010] The invention overcomes the above noted deficiencies of prior repair materials.

[0011] The invention provides a composition that comprises cobalt, chromium, carbon, boron, zirconium, aluminum, at least one refractory material, and nickel that can be used to repair a superalloy article.

[0012] Also, the invention provides a repair process for a superalloy article using a repair material. The repair material comprises cobalt, chromium, carbon, boron, zirconium, aluminum, at least one refractory material, and nickel.

[0013] These and other aspects, advantages and salient features of the invention will become apparent from the following detailed description, which, when taken in conjunction with the annexed drawings, where like parts are designated by like reference characters throughout the drawings, disclose embodiments of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0014]

- 10 Fig. 1 a graphical representation of oxidation resistance curves for known materials and nickel-based repair materials;
- Fig. 2 a graphical representation of oxidation resistance curves for known materials and nickel-based repair materials;
- 15 Fig. 3 is a graphical representation of oxidation resistance curves for nickel-based repair materials; and
- Figs. 4 and 5 are graphical representations of strength as rupture behavior for nickel-based repair materials.

DETAILED DESCRIPTION OF THE DRAWINGS

20 [0015] In the following discussion, the characteristics of each material are discussed in their wrought form, unless otherwise specified. Materials otherwise specified include, but are not limited to, materials provided as a wire, materials provided with an equiaxed microstructure (EA) single structure, and materials provided with directionally solidified (DS) microstructure. Material properties, as discussed herein, are determined under standard industrial tests at the specified conditions, unless otherwise specified. The material compositions set forth herein are provided in approximate atomic percent, unless otherwise discussed.

25 [0016] A repair material, as embodied by the invention, comprises a nickel-based superalloy composition, for example a nickel-based superalloy material with an austenitic nickel (Ni) matrix. The repair material is useful in the repair of structures, including superalloy articles, such as, but not limited to, turbines, blades, airfoils, buckets, vanes, nozzles, and their components (hereinafter "turbine components"). The superalloy of the turbine component comprises known 30 superalloy compositions, including nickel-based superalloys, cobalt-based superalloys, nickel-iron-based superalloys, and other alloys developed for elevated-temperature service, usually based on group VIIIA elements, where the superalloy encounters relatively severe mechanical stressing, and where high surface stability of the superalloy is frequently required.

35 [0017] The austenitic nickel matrix repair materials (hereinafter "nickel-based repair materials") comprise constituents in amounts that maintain and balance the repair material's strength, weldability adherence (a specific or relative measure of a material's ability to be welded under a given set of conditions, so a completed weld part fulfills all functions for which it was intended), and oxidation resistance. The nickel-based repair material comprises at least one refractory element, and comprise gamma prime (γ') in amounts less than about 10 volume percent of the material.

40 [0018] The nickel-based repair material of the invention is metallurgically compatible with a substrate material of a turbine component, such as a superalloy material. Nickel-based repair materials, as embodied by the invention, comprise cobalt (Co), chromium (Cr), carbon (C), boron (B), zirconium (Zr), aluminum (Al), and at least one refractory element including, but not limited to, one of molybdenum (Mo), tungsten (W), rhenium (Re), niobium (Nb), and tantalum (Ta), with a balance (BAL) of the nickel-based repair material comprising nickel (Ni). The ranges (in atomic percent) of each constituent are as follows: cobalt, in a range from about 12.0 to about 15.0; chromium, in a range from about 24.0 to about 30.0; carbon, in a range from about 0.2 to about 3.0; boron, in a range from about 0.02 to about 0.05; zirconium, in a range from about 0.02 to about 0.05; aluminum, in a range from about 0.4 to about 3.0; molybdenum, in a range from about 2.0 to about 7.0; tantalum, in a range from about 0.75 to about 4.0, with the balance nickel. The above 45 refractory element constituents, such as, but not limited to, molybdenum, tantalum, and tungsten, in the nickel-based repair materials promote strengthening, for example solid solution strengthening, of both the repair and turbine component materials.

50 [0019] The nickel-based repair materials comprise at least one additional constituent, including but not limited to, titanium (Ti), and iron (Fe). Additional constituents, if provided in the nickel-based repair materials, are provided in the following atomic percent ranges: niobium, in a range from about 0.6 to about 5.0; titanium, in a range from about 0.25 to about 1.9; rhenium, in a range from about 0.8 to about 1.2; iron, in a range from about 1.9 to about 2.3; and tungsten, in a range from about 1.0 to about 3.0.

55 [0020] Table 1 lists nickel-based repair material ("Materials") compositions, as embodied by the invention, along with known (baseline) nickel-based material compositions, IN617, IN625, and GTD111. The amounts of materials are provided in approximate atomic percents (except as noted), and a balance of the repair material composition comprises

nickel.

TABLE 1

	Material[a/o]	Co	Cr	C	B	Zr	Al	Mo	Ta	OTHER	BAL
5	Material 1	15.0	24.9	0.24	0.03	0.03	2.2	4.3	0.81	0.63Nb 1.84Ti	Ni
10	Material 2	15.0	25.7	0.25	0.03	0.02	1.7	6.5	2.0	1.28Ti	Ni
15	Material 3	15.0	27.0	0.25	0.03	0.02	1.0	7.0	4.0		Ni
20	Material 4	15.0	27.5	0.25	0.03	0.02	1.2	6.0	2.5	5.0Nb 1.5Re	Ni
25	Material 5	15.0	24.7	0.25	0.03	0.02	2.0	2.5	3.0		Ni
30	Material 6	15.0	24.7	0.25	0.03	0.02	2.0	5.0	3.0		Ni
35	Material 7	15.0	24.7	0.25	0.03	0.02	2.0	5.0	3.0	1.0Re 1.0W	Ni
40	Material 8	15.0	24.7	0.25	0.03	0.02	3.0	5.0	1.5		Ni
45	Material 9	15.0	24.7	0.25	0.03	0.02	2.0	5.0	3.0	3.0W	Ni
50	Material 10	15.0	24.7	0.25	0.03	0.02	2.0	5.0	4.0	3.0W	Ni
55	Material 11	15.0	24.7	0.25	0.03	0.02	2.0	6.0	3.0	3.0W	Ni
	Material A	15.0	24.7	0.27	0.03	0.02	2.0	5.5	3.5	2.0W	Ni
	Material B	15.0	24.7	0.27	0.03	0.02	2.0	5.5	3.5	1.25Mn 2.0W 1.0Si	Ni
	Material C	15.0	24.7	0.27	0.03	0.02	2.0	5.5	3.5	1.25Mn 2.0W 2.0Si	Ni
	Material D	15.0	24.7	0.27	0.03	0.02	2.0	5.0	4.0	1.25Mn 3.0W 1.0Si	Ni
	Material E	15.0	24.7	0.27	0.03	0.02	2.0	5.0	4.0	1.25Mn 3.0W 2.0Si	Ni
	Material F	10.2	23.0				2.2	6.2		0.8W	Ni
	IN625		24.64	0.25			0.44	5.6		2.1Fe 0.25Ti 2.3Nb	Ni
	IN617	12.4	24.7	0.3			2.2	5.5			Ni
	GTD111 (weight percent)	9.3	15.5	0.5	0.05		6.4	0.9	0.9	1.2W 5.9Ti	Ni

[0021] The nickel-based repair materials, as embodied by the invention, exhibit enhanced oxidation resistance, which is comparable and often superior to known repair materials. Chromium, aluminum, manganese, and silicon con-

stituents in the nickel-based repair material) both individually and in combination, enhance oxidation resistance of the nickel-based repair materials. Silicon and manganese additions also promote enhanced resistance to oxide spallation. Table 2 is a listing of oxidation characteristics in weight change per area (mg/cm^2) for selected repair materials at about 2000°F (1093°C).

5

TABLE 2

Hrs. at 2000°F	GTD111 wire	GTD111 ea	IN625 wire	DS IN625	Mtl.1	Mtl.5	Mtl.6	Mtl.7	Mtl.8	IN617 wire	
10	24	-3.5	-1.4	-2.1	-11.9	1.4	-0.7	-1.2	0.1	-0.7	0.7
	48	-6.7	-4.7	-2.1	-70.0	1.4	0.2	-0.7	0.3	0.5	0.7
	72	-9.7	-6.1	-6.1		0.9	0.6	-0.1	-0.5	0.6	0.2
	141	-16.1	-10.1	-15.7		0.3	0.8	-0.3	-0.7	0.6	0.0
15	237	-19.4	-14.9	-37.6		-0.8	-1.5	-1.7	-1.5	-0.3	
	309	-24.0	-18.0	-67.0		-9.7	-5.1	-3.2	-3.6	-1.7	-1.2
	405	-28.3	-23.7	-112.0		-58.0	-10.1	-15.9	-8.9	-4.1	-1.9
	477	-32.6	-29.0	-149.0		-104	-13.7	-9.2	-14.0	-6.8	-3.4
20	573	-41.6	-37.2	-180.0		-160	-17.4	-13.8	-20.3	-11.2	-7.0
	645	-58.4	-44.1				-19.3	-17.1	-28.6	-15.9	-10.4
	741	-88.6	-56.6				-22.6	-20.8	-47.0	-21.0	-13.8
	813	-119.0	-67.7				-24.2	-28.1	-73.0	-25.9	-15.9
25	909	-121.0	-80.8				-26.4	-45.4	-91.9	-32.1	-18.5
	1002	-137.0	-99.5				-33.1	-70.1	-103	-42.0	-22.3

[0022] Figures 1 and 2 are graphical representations of oxidation resistance curves for known materials and nickel-based repair materials, as embodied by the invention. Figure 3 is a graphical representation of oxidation resistance curves for Materials A-F as a function of exposure time at about 2000°F (1093°C). The oxidation curves illustrate weight change per area for oxidation versus time at about 2000°F (1093°C). The known materials comprise IN625, GTD111, and IN617, and are provided in wire and wrought forms, and with directionally solidified (DS) and equiaxed (EA) structures, as indicated.

[0023] The nickel-based repair materials, as embodied by the invention, (with the exception of repair material Material 1) exhibit oxidation resistance, which is similar to or enhanced when compared to the oxidation resistance of GTD111. (The oxidation resistance properties of Materials 2-4 are similar to Material 1, and are not illustrated.) The nickel-based repair materials lose minor amounts of material that make them suitable for high temperature applications, such as found in turbine applications. Material 6 exhibits reduced oxidation, about a $30 \text{ mg}/\text{cm}^2$ loss in about 850 hours at about 2500°F (1093°C), where a similar IN625 loss occurs in about 150 hours under similar conditions.

[0024] Materials D and E exhibit beneficial oxidation resistance results due to increased silicon amounts in the nickel-based repair material. Increased molybdenum amounts enhance oxidation resistance for Material E, as compared to oxidation resistance of Material A. Material E provides desirable oxidation resistance for a repair material and for use in a repair process. For example, nickel-based repair material Material E possesses enhanced oxidation resistance, where it loses only about $30 \text{ mg}/\text{cm}^2$ in about 1000 hours of oxidation at about 2000°F (1093°C). By comparison, IN625 loses about a similar material amount in less than only about 150 hours of oxidation at about 2000°F (1093°C), and GTD111 loses a similar material amount in only about 500 hours of oxidation at about 2000°F (1093°C).

[0025] In addition to the enhanced oxidation resistance, the nickel-based repair materials, as embodied by the invention, possess desirable strengths, such as an enhanced rupture strength. The high rupture strength enhances the breakage resistance of the repair material. The desirable rupture strength in nickel-based superalloys may be reduced by materials added to enhance oxidation resistance. Accordingly, material amounts added to superalloys are provided in amounts to obtain enhanced oxidation resistance and enhanced strengths.

[0026] Rupture strengths of superalloy repair materials can be adversely effected by high amounts of manganese and silicon. For example, Materials A, B, and C possess rupture lives that fall in a range from about 68 hours to about 98 hours when tested with a rupture test at about 2000°F(1093°C)/3ksi in air due to increased amounts of manganese

and silicon. Thus, manganese and silicon amounts in superalloy repair materials are provided in amounts that achieve desirable enhanced rupture strengths with enhanced oxidation resistance.

[0027] Figs. 4 and 5 are graphical representations of strength as rupture behavior (stress versus Larson Miller parameter $P_{LM} = T(c + \log t)$ [$c = 20$, T in $^{\circ}$ R, t in hours]) for nickel-based repair materials, as embodied by the invention. The graphs also illustrate rupture behavior curves for DS IN625 and DS IN617 materials and gamma prime (γ') strengthened superalloys, such as, but not limited to, Rene 80 and Rene 41 (trademark General Electric Company). Rupture strength is determined at sample gage centers using tests known in the art.

[0028] Fig. 4 illustrates rupture behavior curves for DS Materials 1, 5, and 6 and Fig. 5 illustrates rupture behavior curves for DS Materials 2, 3, 4, 9, 10 and 11, compared to DS IN625 and DS IN617. The rupture behavior curves indicate enhanced rupture strengths for nickel-based repair materials, as embodied by the invention, compared to DS IN625 and DS IN617. Repair material lifetimes, under rupture tests at 2000°F (1093°C)/3ksi in air for materials are as follows: DS IN617 about 160 hrs.; Material 9 about 77 hrs.; Material 10 about 198 hrs.; Material 11 about 186 hrs.; Material 2 about 67 hrs.; Material 3 about 68 hrs.; and Material 4 about 37 hrs.

[0029] In addition to the enhanced oxidation resistance, repair material DS Material 6 possesses reduced weld cracking frequency and extended rupture life during rupture tests at 2000°F/3ksi. The rupture life of DS Material 6 is about six times longer than a rupture life of DS IN625 material under the same conditions.

[0030] Table 3 provides strength, ductility, and oxidation data for Materials A-F, as embodied by the invention. The nickel-based repair materials, Materials A-F remain relatively ductile, which is desirable for a turbine repair material, as the material is easily worked during the repair process. Their strength is enhanced and both nickel-based repair materials Materials D and E exhibit strengths at least equivalent to known superalloy materials at 2000°F (1093°C)/3ksi.

TABLE 3

	Strength	Ductility	Rupture	Oxidation
Material	YS/UTS 1800°F-ksi	%el/RA 1800°F	2000F/3ksi (hours)	Loss @ 1000hr/2000°F
Material A	23/23	76/80	79.3	>200mg/cm ²
Material B	21/23	80/90	97.2	55
Material C	19/24	62/82	68.2	40
Material D	19/21	91/89	211.7	160
Material E	22/29	61/81	337.4	30
Material F	18/20	103/92	40.1	150

[0031] The rupture behavior of Materials D and E, as embodied by the invention, indicates enhanced strengths from increased amounts of tungsten and tantalum (compared with Materials B and C). The rupture life of directionally solidified Material E is approximately twice the life of a directionally solidified IN617 and is approximately equal to the life of an equiaxed gamma prime (γ') strengthened Rene 80 under rupture tests at 2000°F (1093°C)/3ksi. Material E fails in rupture tests at 3ksi in air after about 335 hours at about 2000°F (1093°C). Comparatively, a directionally solidified IN625 material fails after only about 50 hours, while a directionally solidified IN617 fails after only about 160 hours, in rupture tests under similar conditions. Material E also provides reduced cracking frequency when used in an unconstrained weld repair process, on a turbine component such as a turbine component formed of GTD111. The nickel-based repair Material E, as an unconstrained weld, does not exhibit cracking after heat treatments. In constrained welds, cracking occurs.

[0032] In a superalloy article repair process, the repair material, as embodied by the invention, is provided in the appropriate form for the repair process. For example, and in no way limiting of the invention, if the repair process comprises grinding a damaged tip to a depth approximately equal to a turbine component tip cover plane. A new turbine component tip is built up on the cover plane by a multiple weld-pass repair process with a wire repair material formed from the repair material, as embodied by the invention. The repair material is fed as a wire into a liquid weld pool on the turbine component tip as the weld torch is traversed around the bucket perimeter to form a new tip. Further, the repair material may be fed into a weld pool at a defect in a turbine component, and re-solidified with the turbine component to repair the turbine component. The scope of the repair process, as embodied by the invention, using the repair material, as embodied by the invention, comprises any appropriate repair process that employs repair material.

[0033] While various embodiments are described herein, it will be appreciated from the specification that various combinations of elements, variations or improvements therein may be made by those skilled in the art, and are within the scope of the invention.

Claims

1. A composition comprising:

5 cobalt;
 chromium;
 carbon;
 boron;
 zirconium;
 10 aluminum;
 at least one refractory material; and
 nickel.

2. The composition of claim 1, wherein the composition, in approximate atomic percent, comprises;

15 cobalt, in a range from about 10.0 to about 15.0;
 chromium, in a range from about 24.0 to about 30.0;
 carbon, in a range from about 0.2 to about 0.3;
 boron, in a range from about 0.02 to about 0.05;
 20 zirconium, in a range from about 0.02 to about 0.05;
 aluminum, in a range from about 0.4 to about 3.0;
 at least one refractory material, selected from the group comprising molybdenum, tantalum, tungsten, niobium and rhenium, in a range from about 0.75 to about 7.0; and
 nickel, as a balance of the composition.

25 3. The composition according to claim 1, wherein refractory material comprises at least one of molybdenum and tantalum.

30 4. The composition according to claim 3, wherein the molybdenum is provided in a range from about 2.0 to about 7.0 atomic percent and tantalum is provided in a range from about 0.75 to about 4.0 atomic percent.

35 5. The composition according to claim 1, wherein the refractory material comprises at least one of molybdenum, tungsten, and tantalum.

40 6. The composition according to claim 5, wherein the molybdenum is provided in a range from about 2.0 to about 7.0 atomic percent, tungsten is provided in a range from about 1.0 to about 3.0 atomic percent, and tantalum is provided in a range from about 0.75 to about 4.0 atomic percent.

45 7. The composition according to claim 1, further comprising at least one of manganese, niobium, titanium, rhenium, and silicon.

50 8. The composition according to claim 7, wherein niobium is provided in a range from about 0.6 to about 5.0 atomic percent, titanium is provided in a range from about 0.25 to about 1.9 atomic percent, rhenium is provided in a range from about 0.8 to about 1.2 atomic percent, silicon is provided in a range from about 1.0 to about 2.0 atomic percent, and manganese is provided at about 1.25 atomic percent.

55 9. The composition according to claim 1, wherein the refractory material comprises molybdenum and tantalum, and the composition further comprises niobium and titanium.

50 10. The composition according to claim 1, wherein the refractory material comprises molybdenum and tantalum, and the composition further comprises titanium.

55 11. The composition according to claim 1, wherein the refractory material comprises molybdenum and tantalum, and the composition further comprises niobium and rhenium.

55 12. The composition according to claim 1, wherein the refractory material comprises molybdenum and tantalum, and the composition further comprises rhenium and tungsten.

13. The composition according to claim 1, wherein the refractory material comprises molybdenum, tungsten, and tantalum and the composition further comprises manganese and silicon.
- 5 14. The composition according to claim 1, wherein the refractory material comprises molybdenum and tantalum, the composition comprising cobalt at about 15.0 atomic percent, chromium at about 24.7 atomic percent, carbon at about 0.25 atomic percent, boron at about 0.03 atomic percent, zirconium at about 0.02 atomic percent, aluminum at about 2.0 atomic percent, molybdenum at about 5.0 atomic percent, tantalum at about 3.0 atomic percent, and nickel as a balance.
- 10 15. The composition according to claim 1, the composition further comprising silicon, tungsten and manganese, and the refractory material comprises molybdenum and tantalum, the composition comprising cobalt at about 15.0 atomic percent, chromium at about 24.7 atomic percent, carbon at about 0.27 atomic percent, boron at about 0.03 atomic percent, zirconium at about 0.02 atomic percent, aluminum at about 2.0 atomic percent, molybdenum at about 5.0 atomic percent, tantalum at about 4.0 atomic percent, 1.25 manganese, 3.0 tungsten, 2.0 silicon, and nickel as a balance.
- 15 16. The composition according to claim 1, wherein the composition comprises γ' amounts less than about 10 volume percent of the composition.
- 20 17. A repair material for repairing superalloy articles, the repair material comprising the composition of any preceding claim.
18. A superalloy article comprising a repair material, the repair material possessing a repair material according to claim 17.
- 25 19. A repair process for repairing a superalloy article, the repair process comprising:
 - providing a repair material; and
 - joining the repair material to the superalloy article, the repair material comprising the composition of any one of claims 1 to 16.
20. The process according to claim 19, wherein the superalloy article comprises a turbine component.
- 30 21. The process according to claim 19, wherein the turbine component comprises at least one of a nickel-based superalloy, a nickel-iron based superalloy, and a cobalt-based superalloy

40

45

50

55

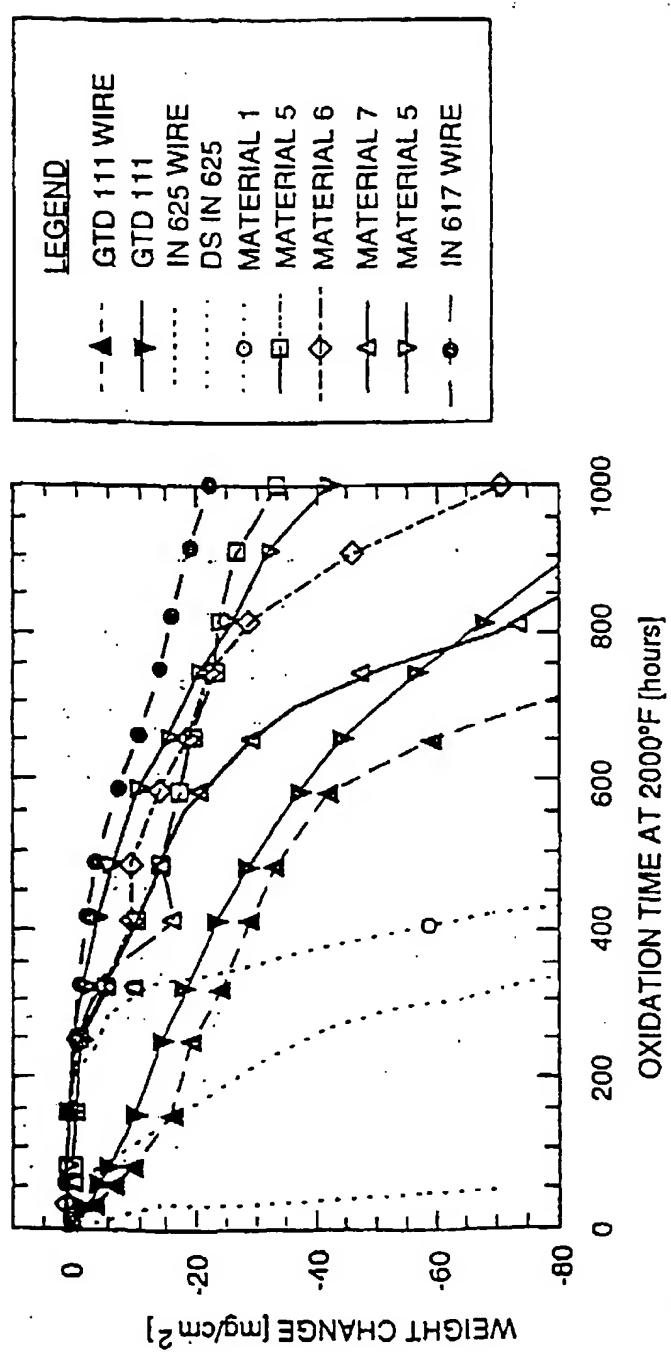


FIG. 1

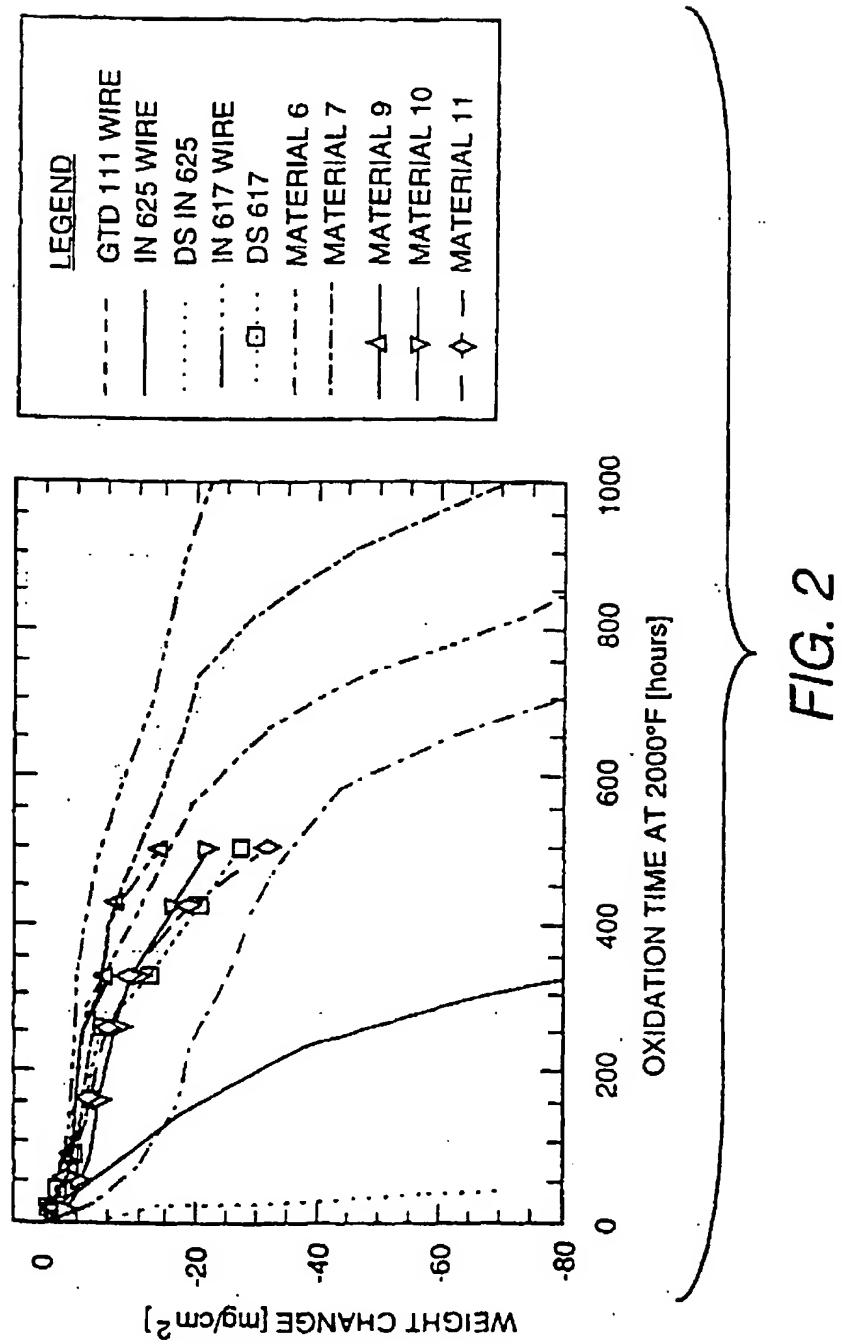


FIG. 2

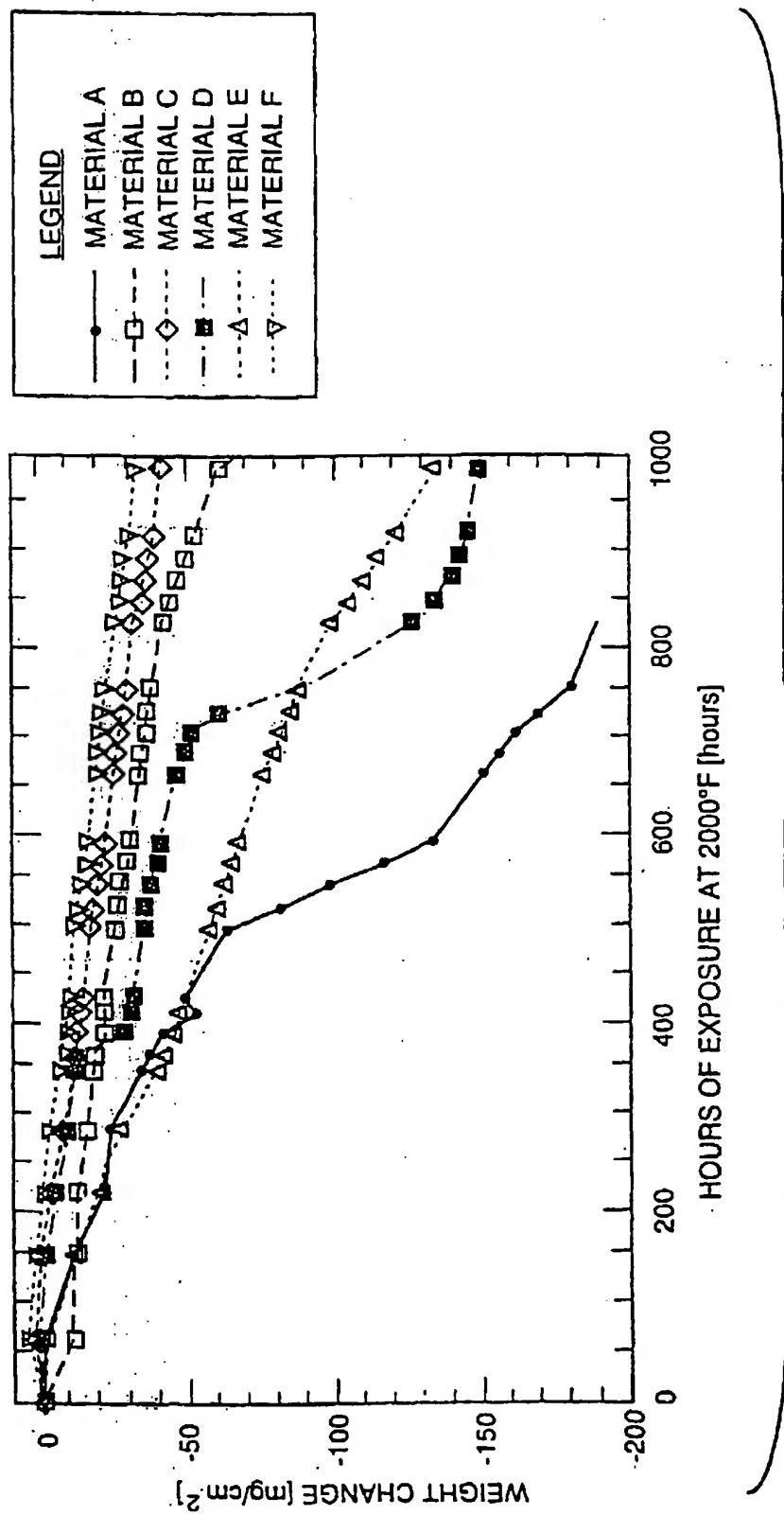


FIG. 3

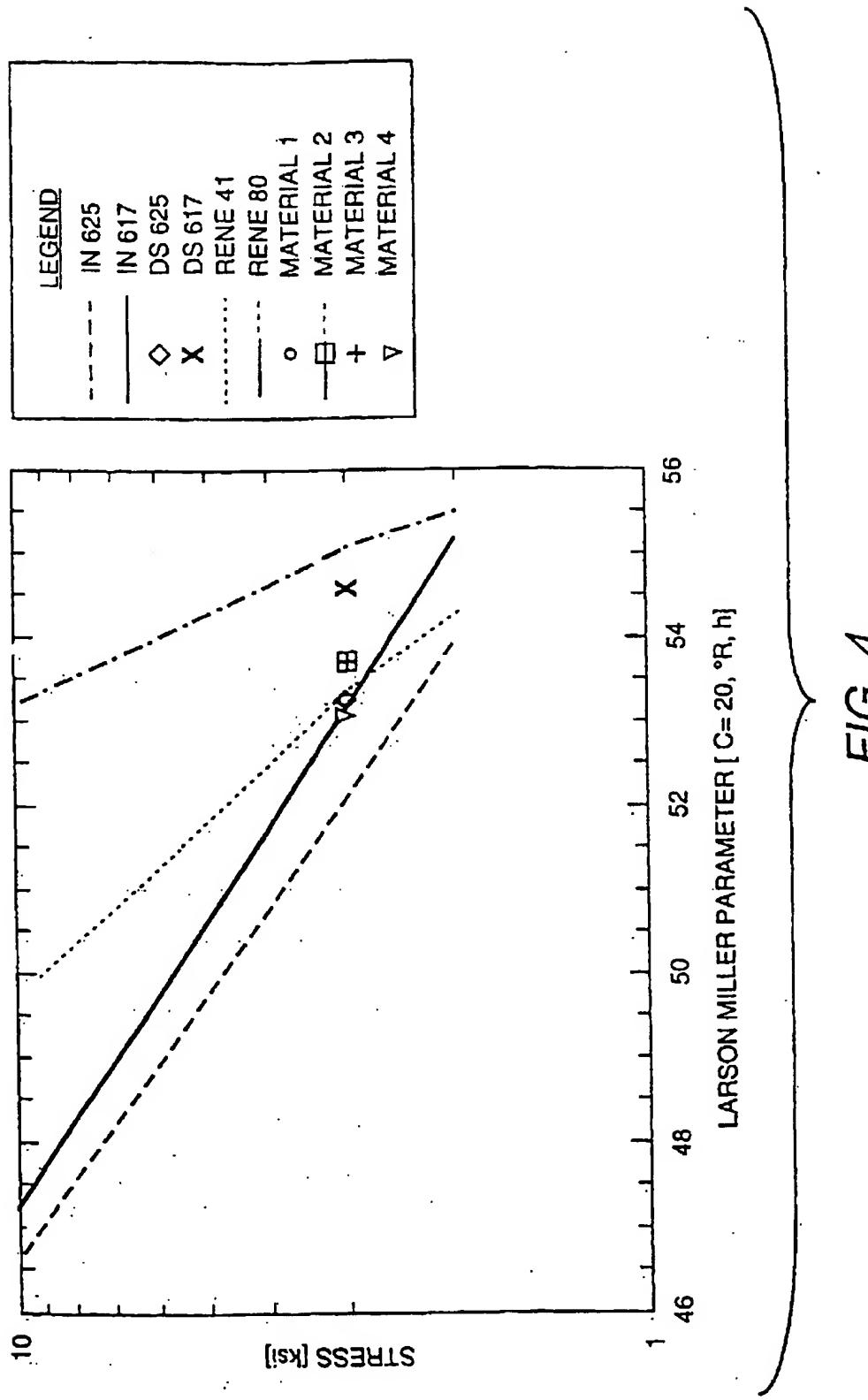
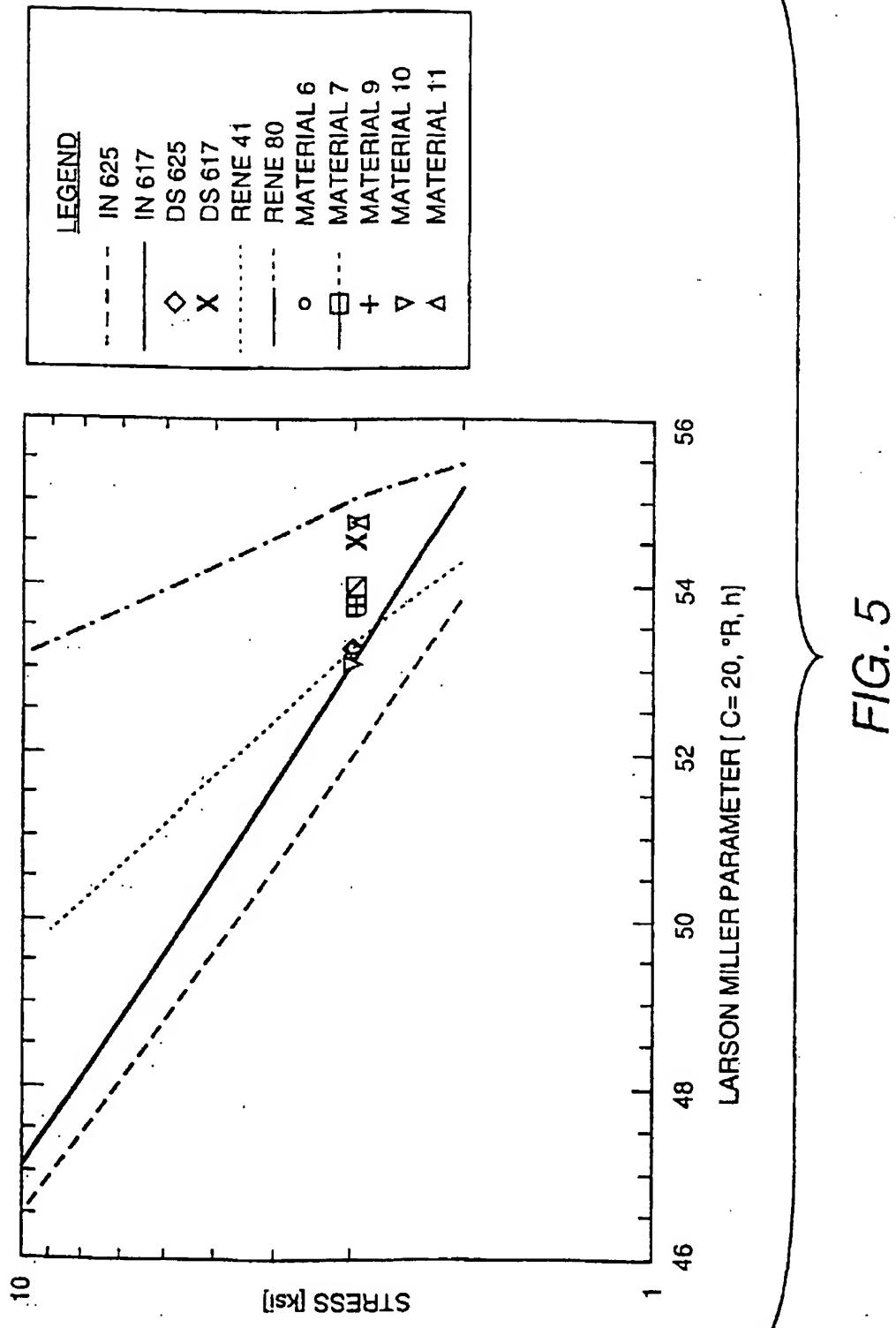


FIG. 4





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 99 30 8723

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	EP 0 302 302 A (GEN ELECTRIC) 8 February 1989 (1989-02-08) * table 1 * ---	1-21	C22C19/05 B23K35/30
X	DE 38 13 157 A (BBC BROWN BOVERI & CIE) 15 December 1988 (1988-12-15) *col.5 and col.8* ---	1-21	
X	GB 2 024 858 A (INCO EUROP LTD) 16 January 1980 (1980-01-16) * table 1 * ---	1-16	
A	EP 0 800 889 A (GEN ELECTRIC) 15 October 1997 (1997-10-15) ---	1-21	
A	EP 0 351 948 A (ROLLS ROYCE PLC) 24 January 1990 (1990-01-24) -----	1-21	
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
			C22C B23K
<p>The present search report has been drawn up for all claims</p>			
Place of search	Data of completion of the search	Examiner	
MUNICH	22 March 2000	Badcock, G	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 99 30 8723

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report.
 The members are as contained in the European Patent Office EDP file on
 The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

22-03-2000

Patent document cited in search report	Publication date	Patent family member(s)			Publication date
EP 0302302 A	08-02-1989	US 4810467 A			07-03-1989
		CA 1333342 A			06-12-1994
		DE 3871018 A			17-06-1992
		JP 1104738 A			21-04-1989
		JP 2716065 B			18-02-1998
DE 3813157 A	15-12-1988	NONE			
GB 2024858 A	16-01-1980	CA 1140780 A			08-02-1983
		CH 643302 A			30-05-1984
		IT 1118876 B			03-03-1986
		JP 1441251 C			30-05-1988
		JP 55008500 A			22-01-1980
		JP 62049342 B			19-10-1987
		US 4288247 A			08-09-1981
EP 0800889 A	15-10-1997	US 5902421 A			11-05-1999
		JP 10029088 A			03-02-1998
EP 0351948 A	24-01-1990	AU 613205 B			25-07-1991
		AU 3678489 A			18-01-1990
		CA 1332299 A			11-10-1994
		DE 68908980 D			14-10-1993
		DE 68908980 T			20-01-1994
		JP 2138432 A			28-05-1990
		JP 2924908 B			26-07-1999
		SG 121593 G			21-01-1994
		US 4940566 A			10-07-1990

EPO FORM P059

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82